

Electro-static drives (ESD) for the AEI-10m prototype

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Original idea: Ken Strain

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Motivation for a new ESD design

The AEI-10m interferometer will face a new problem in terms of the required length actuators for the main optics:

- Beam size at the test masses is driven by demanding thermal noise requirements.
- Beam uses the full mirror size (mirror is only 2.5 times larger than beam \Rightarrow even for optimal centering we have 4 ppm clipping losses).
- ITM and IETM have significant transmission. Therefore we need to have actuators featuring a free aperture of at least mirror size. \Rightarrow **cannot use the GEO design.**

Motivation for a new ESD design

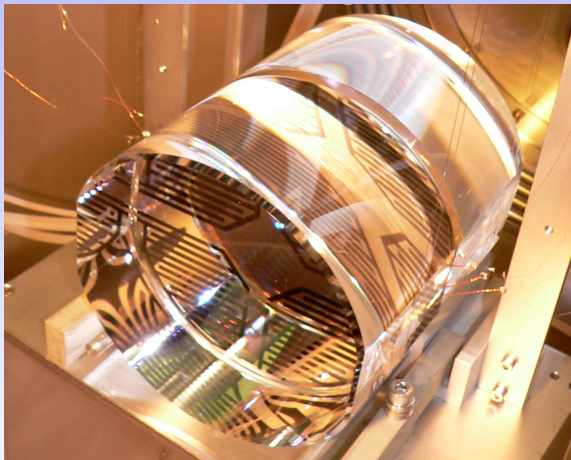


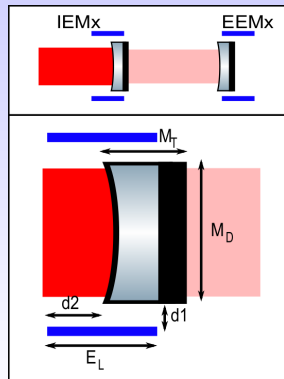
Figure: GEO ESDs

Motivation for a new ESD design

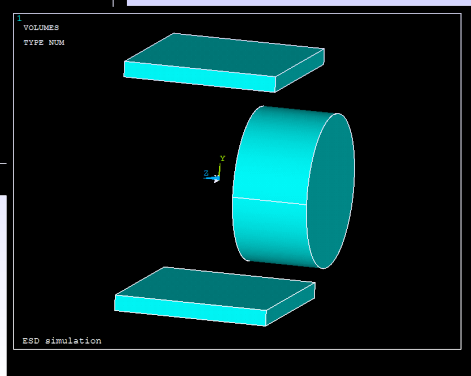
Idea

Use ESDs made of two plates (see picture)

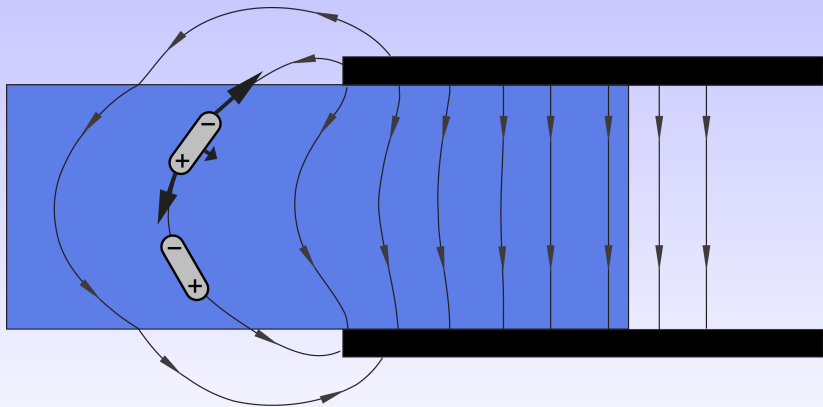
- very large free aperture
- setup where the force is independent of the relative position of ESD and mirror, but just depends on the ESD voltage?!
- **This means very relaxed requirements for the seismic isolation of the ESDs.** Perhaps we could even just bolt them down to the tables?



ESD Design



Origin of the force



Analytical approximation

Assumption: big plates, small gap

$$F = (\epsilon - \epsilon_0) \cdot \omega \cdot U^2 / 2d$$

$U \hat{=}$ voltage

$\omega \hat{=}$ plate depth

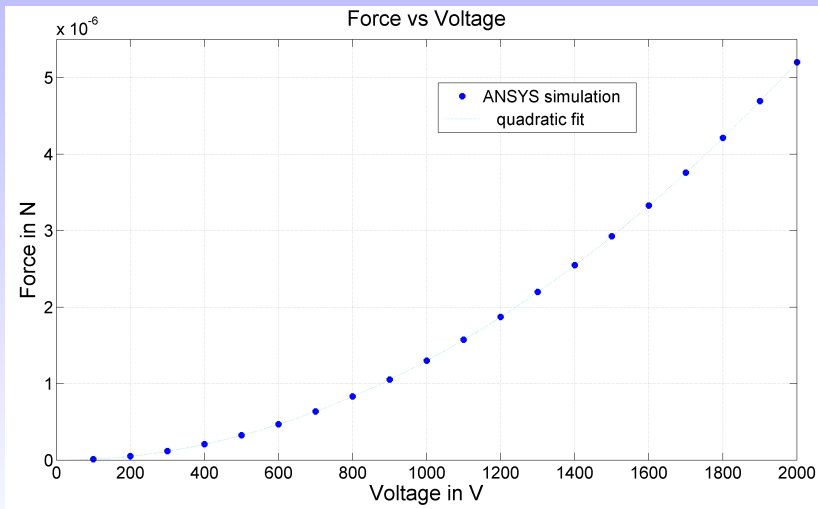
$d \hat{=}$ plate distance

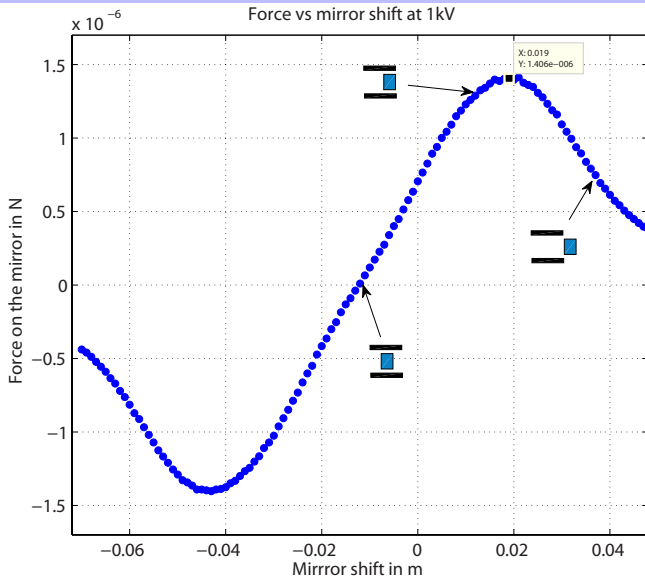
Handwritten calculations on graph paper:

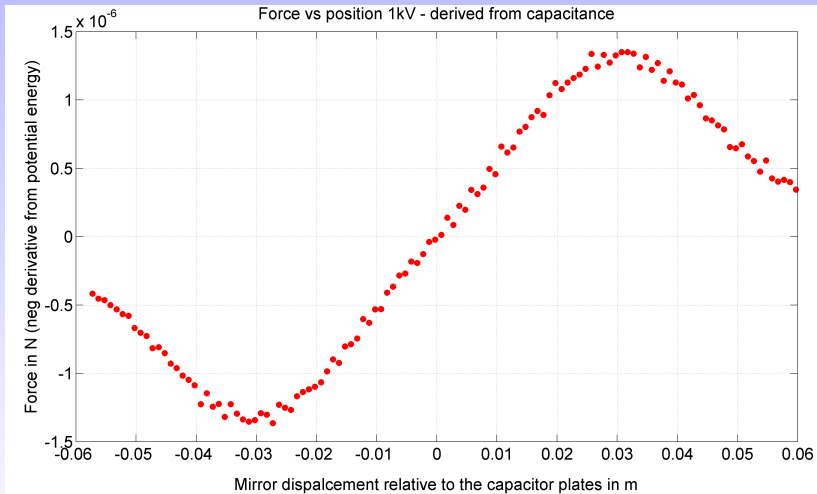
- $$A_m = \pi r^2 = \pi (2.45 \text{ cm})^2 \approx 18.9 \text{ cm}^2$$

$$\epsilon_r \approx 3.7$$
- $$A_p = 5 \text{ cm} \cdot 1 \text{ cm} = 5 \text{ cm}^2$$

$$\epsilon_r = 1$$
- $$\frac{A_m}{A_p} \approx \frac{18.9}{5} \approx 3.78$$
- $$\Rightarrow \epsilon_{\text{eff}} \approx 3.78 \cdot 3.7 \approx 14$$
- $$F_e = \frac{(\epsilon - \epsilon_0) \cdot \omega \cdot U^2}{2d} = \frac{(2.45 - 1) \cdot 8.85 \cdot 10^{-12} \text{ F/m} \cdot 0.05 \text{ m} \cdot (200 \text{ V})^2}{2 \cdot 0.001 \text{ m}}$$
- $$= \frac{8.85 \cdot 5 \cdot 10^{-8} \text{ V}^2 \text{ F}}{14 \cdot 10^{-2} \text{ m}}$$
- $$\approx 3.16 \cdot 10^{-6} \text{ N}$$

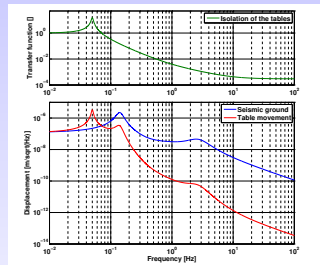
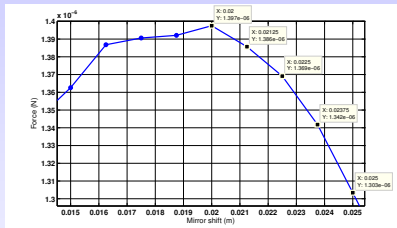






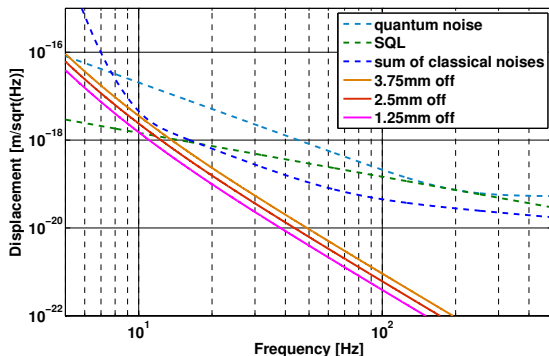
Coupling of seismic for mispositioned ESD

Key-Question: How accurately do we have to position the ESD relative to the mirror in order to not spoil the sensitivity of the AEI-10m?



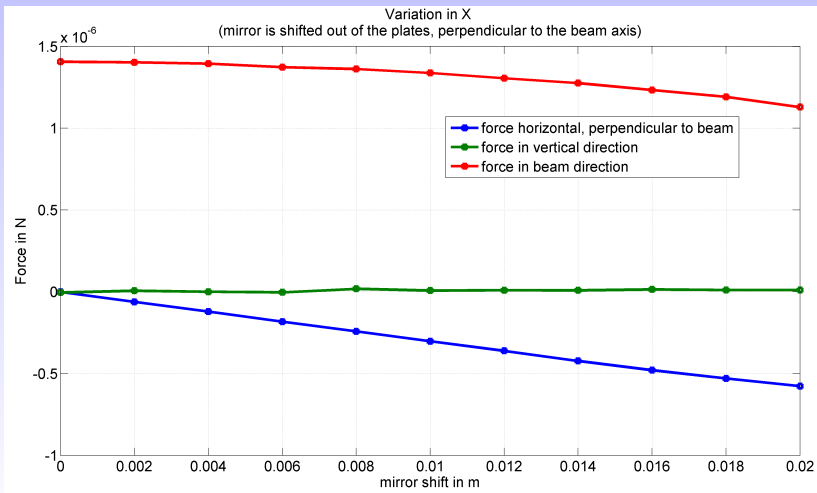
Calculation: Assume some deviation from optimal positions. Take corresponding slope from force vs position plot. Then fold it be the expected movement of the tables (seismic and table transferfunction taken from labbook 205).

Coupling of seismic for mispositioned ESD: Result

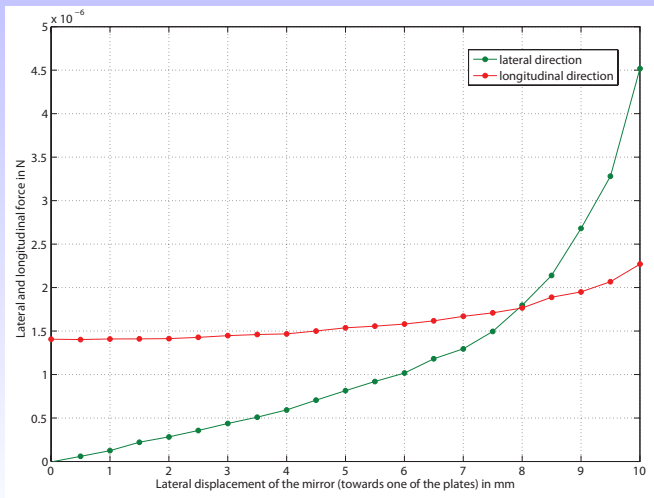


Assuming that the table performance will be achieved and that we are able to position the mirror and ESD in respect to each other within a few millimeter, noise wise it would be ok to mount the ESDs directly onto the tables.

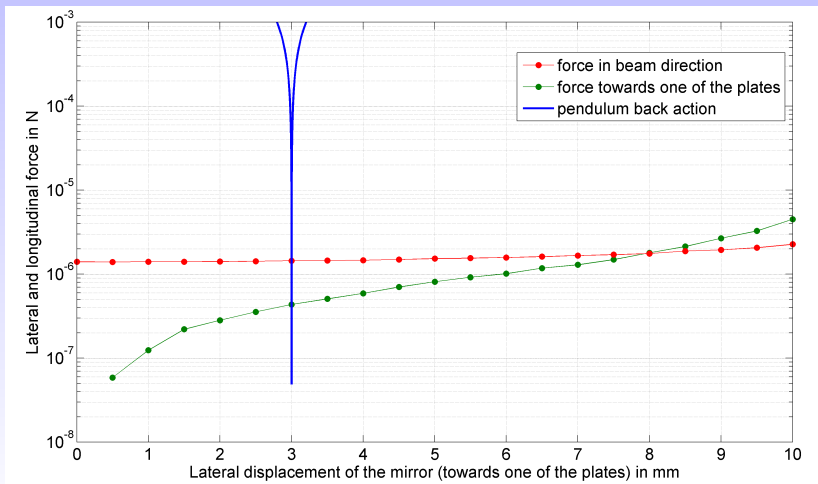
Miscentering out of the plates



Miscentering towards plates



Miscentering towards plates



Conclusion

Conclusion:

- GEO-style ESDs are not suitable for the prototype
⇒ therefore we investigated a plate ESD design

Generally the force on the mirror depends on its position

But there is a maximum! ⇒ Operating point

- Plate ESDs provide forces in the order of micro N
- They could be directly mounted onto the tables in terms of noise

Outlook

Things to be done:

- Look at various type of tolerances ...
- Look test mass rotation and tilt ...
- charged testmass ...